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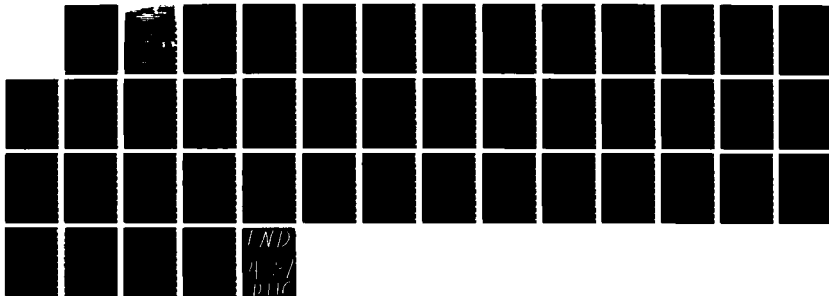
COMPUTER PROGRAM FOR ELECTROMAGNETIC PENETRATION INTO A 1/1
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ELECTRICAL AND COMPUTER ENGINEERING. J R MAUTZ ET AL.

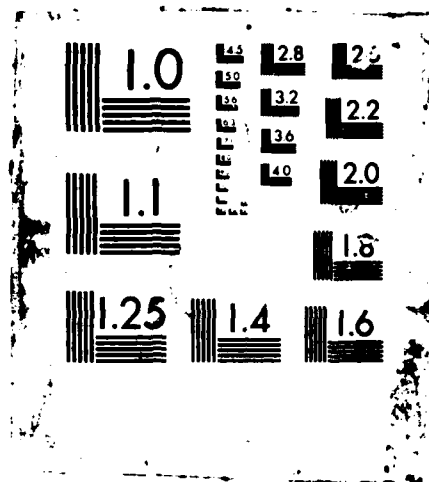
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COMPUTER PROGRAM FOR
ELECTROMAGNETIC PENETRATION INTO A CONDUCTING
CIRCULAR CYLINDER THROUGH A
NARROW SLOT, TM CASE

Interim Technical Report No. 7

by

Joseph R. Mautz

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February 1987

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A computer program is described and listed. This program calculates electromagnetic penetration of a TM plane wave into the cylindrical cavity for which $\rho \leq a$ when the surface ($\phi = a$, $\phi_0 \leq \phi \leq 2\pi - \phi_0$) is perfectly conducting. Here, ρ and ϕ are cylindrical coordinates. The z directed electric field E_z in the slot aperture ($\rho = a$, $\phi_0 \leq \phi \leq \phi_1$) is expressed as a linear combination of 4 even and 4 odd expansion functions. The method of moments is used to obtain the coefficients of these functions. The elements of the		

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20. ABSTRACT (continued)

moment matrix are obtained by expressing each expansion function as a Fourier series in ϕ valid for $(0 \leq \phi < 2\pi)$.

Our moment solution remains accurate when the cavity becomes resonant because alternative expansion functions were chosen to prevent the moment matrix from becoming ill-behaved. As the aperture width $2a$ decreases, more and more terms in the Fourier series are needed. Thanks to Debye's asymptotic expansions for Bessel functions, we are able to handle 10,000 terms so as to obtain accurate results for a as small as 1.25.

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INTRODUCTION

In [1], a procedure is presented for calculating the electromagnetic field in the vicinity of an infinitesimally thin perfectly conducting circular cylindrical shell with an infinitely long slot illuminated by a TM wave. A computer program was written to implement this procedure. For the shell of [1, Fig. 1] illuminated by the incident electric field \underline{E}^i given by [1, eq. (1)]

$$\underline{E}^i = \underline{u}_z e^{jk\rho} \cos(\phi - \alpha), \quad (1)$$

the program calculates the amplitude $|E_z|$ of the z directed electric field at equally spaced points in the slot aperture and along the straight line that runs from the center of the cylinder to the center of the aperture. The radius of the shell is a , and the angular width of the slot aperture is $2\phi_0$. The incident electric field is the electric field that would exist if the shell were absent. In (1), (ρ, ϕ, z) are cylindrical coordinates, and \underline{u}_z is the unit vector in the z-direction. The incident wave (1) comes from the direction for which $\phi = \alpha$. In (1), $k = \omega\sqrt{\mu\epsilon}$ where ω is the angular frequency, μ is the permeability of the homogeneous medium that surrounds the shell, and ϵ is the permittivity of this medium.

The computer program consists of the subroutines BES, BESJ, BESJY, BESJJ, SFEO, DECOMP, and SOLVE, and a main program. The main program reads input data on the file MAUTZ3.DAT and writes output data on file MAUTZ6.DAT. The user who wants merely to run the program is advised to skip to Section VIII and to read only the descriptions of the input and output data there.

II. THE SUBROUTINE BES

The subroutine BES(Y_0 , N, X, BJ, BY) puts the Bessel function of the first kind $J_n(X)$ in BJ(n+1) and the Bessel function of the second kind $Y_n(X)$ in BY(n+1) for $n=0,1,\dots,N$ where X is a positive real number. The subroutine BES differs from that in [2, Sec. II] only in that common input variables $Y_0(1)$ to $Y_0(33)$, PI2, PI4, PI7, in [2, p. 6] have been changed to the subroutine arguments $Y_0(1)$ to $Y_0(33)$, $Y_0(34)$, $Y_0(35)$, and $Y_0(36)$, respectively, and the common output variables BJ and BY have been changed to the subroutine arguments BJ and BY, respectively. The symbol 0 in Y_0 denotes zero rather than the letter O. In other instances when it is obvious from the context that a zero is meant, the slash is not used.

Minimum allocations are given by

DIMENSION BJ(N+1), BY(N+1), AJ(11+N+2*[X]) where [X] is the largest integer that does not exceed X.

```

1C  LISTING OF THE SUBROUTINE BES
2  SUBROUTINE BES(YO,N,X,BJ,BY)
3  DIMENSION YO(36),BJ(100),BY(100),AJ(100)
4  NZ=10+N+2*IFIX(X)
5  IF(X.LT.1.E-3) NZ=4+N
6  AJ(NZ+1)=0.
7  AJ(NZ)=1.E-20
8  M1=NZ-1
9  X2=2./X
10 DO 16 K=1,M1
11  MK=NZ-K
12  AJ(MK)=X2*FLOAT(MK)*AJ(MK+1)-AJ(MK+2)
13 16 CONTINUE
14  ALP=.5*AJ(1)
15  DO 15 J=3,NZ,2
16  ALP=ALP+AJ(J)
17 15 CONTINUE
18  ALP=2.*ALP
19  NP=N+1
20  DO 17 K=1,NP
21  BJ(K)=AJ(K)/ALP
22 17 CONTINUE
23  IF(X-8.) 18,18,19
24 18 Z1=X*X
25  Z2=0.
26  Z3=0.
27  Z4=0.
28  Z5=0.
29  Z6=0.
30  Z7=0.
31  IF(Z1.LT.1.E-11) GO TO 22
32  Z2=Z1*Z1
33  Z3=Z2*Z1
34  IF(Z1.LT.1.E-6) GO TO 22
35  Z4=Z3*Z1
36  Z5=Z4*Z1
37  IF(Z1.LT.1.E-4) GO TO 22
38  Z6=Z5*Z1
39  Z7=Z6*Z1
40 22 S=(YO(1)+YO(2)*Z1+YO(3)*Z2+YO(4)*Z3+YO(5)*Z4+YO(6)*Z5+
41  YO(7)*Z6+YO(8)*Z7)/(YO(9)+YO(10)*Z1+YO(11)*Z2)
42  TLG=ALOG(X)
43  BY(1)=S+YO(34)*BJ(1)*TLG
44  IF(N.LE.0) RETURN
45  S=(YO(12)+YO(13)*Z1+YO(14)*Z2+YO(15)*Z3+YO(16)*Z4+
46  YO(17)*Z5+YO(18)*Z6)/(YO(19)+YO(20)*Z1+YO(21)*Z2)
47  BY(2)=X*S+YO(34)*(BJ(2)*TLG-1./X)
48  GO TO 20
49 19 Z=8./X
50  Z1=Z*Z
51  Z2=Z1*Z1
52  S=SQRT(YO(34)/X)
53  S1=YO(22)+YO(23)*Z1+YO(24)*Z2
54  S3=Z*(YO(28)+YO(29)*Z1+YO(30)*Z2)
55  S5=X-YO(35)
56  BY(1)=S*(S1*SIN(S5)+S3*COS(S5))
57  IF(N.LE.0) RETURN
58  S2=YO(25)+YO(26)*Z1+YO(27)*Z2
59  S4=Z*(YO(31)+YO(32)*Z1+YO(33)*Z2)
60  S6=X-YO(36)
61  BY(2)=S*(S2*SIN(S6)+S4*COS(S6))
62 20 IF(NP.LE.2) RETURN
63  DO 21 K=3,NP
64  K2=K-2
65  BY(K)=X2*FLOAT(K2)*BY(K-1)-BY(K2)
66 21 CONTINUE
67  RETURN
68  END

```

III. THE SUBROUTINE BESJ

The subroutine BESJ(X, BJZ, BJ1) puts $J_0(X)$ in BJZ and $J_1(X)$ in BJ1 where X is a positive real number.

If $X \leq 3$, then $J_0(X)$ and $J_1(X)$ are calculated in lines 5 to 20 in the listing of BESJ at the end of this section. As suggested in [3, Sec. 9.12., Example 1], $J_{MZ}(X)$ and $J_{MZ-1}(X)$ are set equal to the arbitrary values of zero and 10^{-20} , respectively, where

$$MZ = 11 + 2[X] \quad (2)$$

where $[X]$ is the largest integer that does not exceed X. This is done in lines 5 to 7. In DO loop 16, the recurrence relation [3, Eq. (9.1.27)]

$$J_n(X) = \frac{2(n+1)}{X} J_{n+1}(X) - J_{n+2}(X) \quad (3)$$

is used to calculate $\{J_n(X), n = MZ-2, MZ-3, \dots, 0\}$. Line 12 puts $J_{MK-1}(X)$ in BJ(MK). According to [3, eq. (9.1.46)], the calculated values of $J_0(X)$ and $J_1(X)$ have to be normalized by dividing by α where

$$\alpha = J_0(X) + 2J_2(X) + 2J_4(X) + \dots \quad (4)$$

The division by α is performed in lines 19 and 20.

If $X > 3$, then $J_0(X)$ and $J_1(X)$ are calculated in lines 22 to 38. The polynomial approximations [3, Eqs. 9.4.3 and 9.4.6] are used. With regard to [3, Eq. 9.4.3], lines 28 and 29 put f_0 in FZ, lines 30 and 31 put θ_0 in TZ, and line 37 puts $J_0(X)$ in BJZ. With regard to [3, Eq. 9.4.6], lines 32 and 33 put f_1 in F1, lines 34 and 35 put θ_1 in T1, and line 38 puts $J_1(X)$ in BJ1.

```

1C  LISTING OF THE SUBROUTINE BESJ
2  SUBROUTINE BESJ(X,BJZ,BJ1)
3  DIMENSION BJ(18)
4  IF(X-3.) 17,17,18
5  17 NZ=11+2*IFIX(X)
6  BJ(NZ+1)=0.
7  BJ(NZ)=1.E-20
8  N1=NZ-1
9  X2=2./X
10 DO 16 K=1,N1
11  NK=NZ-K
12  BJ(NK)=X2*FLOAT(NK)*BJ(NK+1)-BJ(NK+2)
13 16 CONTINUE
14  ALP=.5*BJ(1)
15  DO 19 J=3,NZ,2
16  ALP=ALP+BJ(J)
17 19 CONTINUE
18  ALP=2.*ALP
19  BJZ=BJ(1)/ALP
20  BJ1=BJ(2)/ALP
21  RETURN
22 18 X1=3./X
23  X2=X1*X1
24  X3=X2*X1
25  X4=X3*X1
26  X5=X4*X1
27  X6=X5*X1
28  FZ=.7978846-.77E-6*X1-.55274E-2*X2-.9512E-4*X3+
29  1.137237E-2*X4-.72805E-3*X5+.14476E-3*X6
30  TZ=X-.7853982-.4166397E-1*X1-.3954E-4*X2+.262573E-2*X3-
31  1.54125E-3*X4-.29333E-3*X5+.13558E-3*X6
32  F1=.7978846+.156E-05*X1+.1659667E-01*X2+.17105E-03*X3-
33  1.249511E-02*X4+.113653E-02*X5-.20033E-03*X6
34  T1=X-2.356194+.1249961*X1+.565E-04*X2-.637879E-02*X3+
35  1.74348E-03*X4+.79824E-03*X5-.29166E-03*X6
36  XX=SQRT(X)
37  BJZ=FZ/XX*COS(TZ)
38  BJ1=F1/XX*COS(T1)
39  RETURN
40  END

```

IV. THE SUBROUTINE BESJY

The subroutine BESJY(N, X, BJY) puts $J_N(X)$ $Y_N(X)$ in BJY where J_N and Y_N are, respectively, the Bessel functions of the first and second kinds of order N. Here, X is a non-negative real number, and N is large enough so that Debye's asymptotic expansions [3, eqs. (9.3.7) and (9.3.8)] apply to $J_N(X)$ and $Y_N(X)$. The subroutine BESJY is that in [2, Sec. VI] with DO loop 11 removed, the arguments N1 and N2 replaced by N, and the array BJY replaced by the single variable BJY.

```

1C  LISTING OF THE SUBROUTINE BESJY
2  SUBROUTINE BESJY(N,X,BJY)
3  F1=N
4  F2=F1*F1
5  F3=F2*F1
6  F4=F3*F1
7  XN=X/F1
8  T1=1./SQRT(1.-XN*XN)
9  T2=T1*T1
10 T3=T2*T1
11 T4=T3*T1
12 T5=T4*T1
13 T6=T5*T1
14 T7=T6*T1
15 T8=T7*T1
16 T9=T8*T1
17 T10=T9*T1
18 T12=T10*T2
19 U1=(3.*T1-5.*T3)/(24.*F1)
20 U2=(81.*T2-462.*T4+385.*T6)/(1152.*F2)
21 U3=(30375.*T3-369603.*T5+765765.*T7-425425.*T9)/(414720.*F3)
22 U4=(4465125.*T4-9412168.E+01*T6+3499224.E+02*T8-4461857.E+02*
23 1T10+1859107.E+02*T12)/(3981312.E+01*F4)
24 U5=1.+U2+U4
25 U6=U1+U3
26 BJY=-T1/(3.141593*F1)*(U5+U6)*(U5-U6)
27 RETURN
28 END

```

V. THE SUBROUTINE BESJJ

The subroutine BESJJ(N, NR, X, BJJ) puts $\frac{J_N(X(L))}{J_N(X(NR))}$ in BJJ(L) for $L = 1, 2, \dots, NR$. Here, $X(L) \geq 0$ and N is large enough so that Debye's asymptotic expansion applies to J_N . Minimum allocations are given by

DIMENSION X(NR), BJJ(NR), U5(NR), U6(NR)

Consider $J_N(XX)$ where

$$XX = X(L) \quad (5)$$

Debye's asymptotic expansion for $J_N(XX)$ is [3, eq. (9.3.7)]

$$J_N(XX) = \frac{e^{N(\tanh \alpha - \alpha)}}{\sqrt{2\pi N \tanh \alpha}} \left(1 + \sum_{k=1}^4 \frac{u_k(\coth \alpha)}{N^k} \right) \quad (6)$$

where u_k is given by [3, formula 9.3.9] and

$$\tanh \alpha = \sqrt{1 - \left(\frac{XX}{N}\right)^2} \quad (7)$$

From [4, formula 702.], we have

$$\alpha = \frac{1}{2} \ln \left(\frac{1 + \tanh \alpha}{1 - \tanh \alpha} \right) \quad (8)$$

Substituting (7) into (8) and rationalizing the denominator of the argument of the logarithm, we obtain

$$\alpha = \ln \left[\frac{N}{XX} (1 + \tanh \alpha) \right] \quad (9)$$

Substitution of (9) into (6) gives

$$J_N(XX) = \frac{1}{\sqrt{2\pi N \tanh \alpha}} \left(\frac{XX e^{\tanh \alpha}}{N(1 + \tanh \alpha)} \right)^N \left(1 + \sum_{k=1}^4 \frac{u_k(\coth \alpha)}{N^k} \right) \quad (10)$$

Thanks to (10), we obtain

$$\frac{J_N(XX)}{J_N(X(NR))} = \left(\frac{U6(L)}{U6(NR)} \right) \left(\frac{U5(L)}{U5(NR)} \right)^N \quad (11)$$

where

$$U5(L) = \frac{XX e^{\tanh \alpha}}{1 + \tanh \alpha} \quad (12)$$

and

$$U6(L) = \frac{1 + \sum_{k=1}^4 \frac{u_k(\coth \alpha)}{N^k}}{\sqrt{\tanh \alpha}} \quad (13)$$

Here, $\tanh \alpha$ depends on L by means of (7) with XX given by (5).

In the listing of the subroutine BESJJ at the end of this section, line 5 inside DO loop 11 obtains XX of (5). Lines 23 to 26 put u_1 , u_2 , u_3 , and u_4 of (13) in $U1$, $U2$, $U3$, and $U4$, respectively. Line 28 obtains $U5(L)$ of (12). Line 29 obtains $U6(L)$ of (13). Inside DO loop 12, line 34 puts $J_N(XX)/J_N(X(NR))$ of (11) in $BJJ(L)$.

```

1C  LISTING OF THE SUBROUTINE BESJJ
2  SUBROUTINE BESJJ(N,NR,X,BJJ)
3  DIMENSION X(11),BJJ(11),U5(11),U6(11)
4  DO 11 L=1,NR
5  XX=X(L)
6  F1=N
7  F2=F1*F1
8  F3=F2*F1
9  F4=F3*F1
10  XN=XX/F1
11  TT=SQRT(1.-XN*XN)
12  T1=1./TT
13  T2=T1*T1
14  T3=T2*T1
15  T4=T3*T1
16  T5=T4*T1
17  T6=T5*T1
18  T7=T6*T1
19  T8=T7*T1
20  T9=T8*T1
21  T10=T9*T1
22  T12=T10*T2
23  U1=(3.*T1-5.*T3)/(24.*F1)
24  U2=(81.*T2-462.*T4+385.*T6)/(1152.*F2)
25  U3=(30375.*T3-369603.*T5+765765.*T7-425425.*T9)/(414720.*F3)
26  U4=(4465125.*T4-9412168.E+01*T6+3499224.E+02*T8-4461857.E+02*
27  T10+1859107.E+02*T12)/(3981312.E+01*F4)
28  U5(L)=XX*EXP(TT)/(1.+TT)
29  U6(L)=(1.+U1+U2+U3+U4)/SQRT(TT)
30  11 CONTINUE
31  S5=U5(NR)
32  S6=U6(NR)
33  DO 12 L=1,NR
34  BJJ(L)=U6(L)/S6*(U5(L)/S5)**N
35  12 CONTINUE
36  BJJ(NR)=1.
37  RETURN
38  END

```


VI. THE SUBROUTINE SFEO

The subroutine SFEO(N, P, SE, SO, FE, FO) puts S_{JN}^e of [1, eqs. (A-18) to (A-21)] or [1, eqs. (A-32) to (A-35)] in SE(J), S_{JN}^o of [1, eqs. (A-22) to (A-25)] or [1, eqs. (A-37) to (A-40)] in SO(J), F_{JN}^e of [1, eqs. (B-5) to (B-8)] or [1, eqs. (B-18) to (B-21)] in FE(J), and F_{JN}^o of [1, eqs. (B-9) to (B-12)] or [1, eqs. (B-22) to (B-25)] in FO(J), all for $J=1,2,3$, and 4. The variables N and P are input arguments defined by

$$\left. \begin{array}{l} N = n \\ P = \phi_o \end{array} \right\} \quad (14)$$

where n and ϕ_o appear in [1, eq. (B-4)] so that [1, eq. (B-4)] becomes

$$b = N * P \quad (15)$$

The subroutine SFEO calls the subroutine BESJ.

The subroutine SFEO is listed at the end of this section. If $b > 2$, line 11 of this listing puts $J_o(b)$ and $J_1(b)$ in BJZ and BJ1, respectively. Lines 15 to 19 put S_{JN}^e of [1, eqs. (A-18) to (A-21)] in SE(J) for $J=1,2,3$, and 4. Lines 22 to 26 put S_{JN}^o of [1, eqs. (A-22) to (A-25)] in SO(J) for $J=1,2,3$, and 4. Lines 30 to 33 put F_{JN}^e of [1, eqs. (B-5) to (B-8)] in FE(J) for $J=1,2,3$, and 4. Lines 36 to 40 put F_{JN}^o of [1, eqs. (B-9) to (B-12)] in FO(J) for $J=1,2,3$, and 4.

If $b \leq 2$, lines 42 and 43 put $\epsilon_n \phi_o / 2$ in PP. Lines 46 to 53 put S_{JN}^e of [1, eqs. (A-32) to (A-35)] in SE(J) for $J=1,2,3$, and 4. Lines 55 to 62 put S_{JN}^o of [1, eqs. (A-37) to (A-40)] in SO(J) for $J=1,2,3$, and 4. Lines 63 to 70 put F_{JN}^e of [1, eqs. (B-18) to (B-21)] in FE(J) for $J=1,2,3$, and 4. Lines 71 to 78 put F_{JN}^o of [1, eqs. (B-22) to (B-25)] in FO(J) for $J=1,2,3$, and 4.

```

1C  LISTING OF THE SUBROUTINE SFEO
2C  THE SUBROUTINE SFEO CALLS THE SUBROUTINE BESJ.
3    SUBROUTINE SFEO(N,P,SE,SO,FE,FO)
4    DIMENSION SE(4),SO(4),FE(4),FO(4)
5    FN=N
6    B=FN*P
7    B2=B*B
8    B4=B2*B2
9    B6=B4*B2
10   IF(B.LE.2.) GO TO 11
11   CALL BESJ(B,BJZ,BJ1)
12   SZ=BJZ/FN
13   BZ=B*SZ
14   B1=BJ1/FN
15   SE(1)=B1
16   SE(2)=((B2-6.)*B1+3.*BZ)/B2
17   SE(3)=((B4-27.*B2+120.)*B1+6.*(B2-10.)*BZ)/B4
18   SE(4)=((B6-63.*B4+1200.*B2-5040.)*B1+3.*(3.*B4-95.*B2+840.)*B
19   1Z)/B6
20   BZ=SZ
21   B1=B1/B
22   SO(1)=2.*B1-BZ
23   SO(2)=((5.*B2-24.)*B1-(B2-12.)*BZ)/B2
24   SO(3)=((8.*B4-168.*B2+720.)*B1-(B4-39.*B2+360.)*BZ)/B4
25   SO(4)=((11.*B6-537.*B4+9720.*B2-40320.)*B1-(B6-81.*B4+2340.*B
26   12-20160.)*BZ)/B6
27   SN=SIN(B)/FN
28   SS=COS(B)/FN
29   CS=B*SS
30   FE(1)=SN
31   FE(2)=(2.*CS+(B2-2.)*SN)/B2
32   FE(3)=(4.*(B2-6.)*CS+(B4-12.*B2+24.)*SN)/B4
33   FE(4)=(6.*(B4-20.*B2+120.)*CS+(B6-30.*B4+360.*B2-720.)*SN)/B6
34   SN=SN/B
35   CS=SS
36   FO(1)=SN-CS
37   FO(2)=(3.*(B2-2.)*SN-(B2-6.)*CS)/B2
38   FO(3)=(5.*(B4-12.*B2+24.)*SN-(B4-20.*B2+120.)*CS)/B4
39   FO(4)=(7.*(B6-30.*B4+360.*B2-720.)*SN-(B6-42.*B4+840.*B2-5040
40   1.)*CS)/B6
41   RETURN
42 11 PP=P
43   IF(N.EQ.0) PP=.5*PP
44   B8=B6*B2
45   B10=B8*B2
46   SE(1)=PP/2.*(1.-B2/8.+B4/192.-B6/9216.+B8/737280.-B10/884736.
47   1E+02)
48   SE(2)=PP/8.*(1.-B2/4.+B4*5./384.-B6*7./23040.+B8/245760.-B10*
49   111./3096576.E+02)
50   SE(3)=PP/16.*(1.-B2*5./16.+B4*7./384.-B6*7./15360.+B8*11./172
51   10320.-B10*143./2477281.E+03)
52   SE(4)=PP*5./128.*(1.-B2*7./20.+B4*7./320.-B6*11./19200.+B8*14
53   13./172032.E+02-B10*143./1857946.E+03)

```

```

54  PB=P*B
55  S0(1)=PB/8.*(1.-B2/12.+B4/384.-B6/23040.+B8/2211840.-B10/3096
56  1576.E+02)
57  S0(2)=PB/16.*(1.-B2*5./48.+B4*7./1920.-B6/15360.+B8*11./15482
58  188.E+01-B10*13./2477261.E+03)
59  S0(3)=PB*5./128.*(1.-B2*7./60.+B4*7./1600.-B6*11./134400.+B8*
60  1143./1548288.E+02-B10*13./1857946.E+03)
61  S0(4)=PB*7./256.*(1.-B2/8.+B4*11./2240.-B6*143/1505280.+B8*14
62  13./1300562.E+02-B10*17./2000864.E+03)
63  FE(1)=P*(1.-B2/6.+B4/120.-B6/5040.+B8/362880.-B10/399168.E+02
64  1)
65  FE(2)=P/3.*(1.-B2*.3+B4/56.-B6/2160.+B8/147840.-B10/157248.E+
66  102)
67  FE(3)=P/5.*(1.-B2*5./14.+B4*5./216.-B6/1584.+B8/104832.-B10/1
68  108864.E+02)
69  FE(4)=P/7.*(1.-B2*7./18.+B4*7./264.-B6*7./9360.+B8/86400.-B10
70  1/8812800.)
71  F0(1)=PB/3.*(1.-B2*.1+B4/280.-B6/15120.+B8/1330560.-B10/17297
72  128.E+02)
73  F0(2)=PB/5.*(1.-B2*5./42.+B4/216.-B6/11088.+B8/943488.-B10/11
74  197504.E+02)
75  F0(3)=PB/7.*(1.-B2*7./54.+B4*7./1320.-B6/9360.+B8/777600.-B10
76  1/969408.E+02)
77  F0(4)=PB/9.*(1.-B2*3./22.+B4*3./520.-B6/8400.+B8/685440.-B10/
78  1842688.E+02)
79  RETURN
80  END

```

VII. THE SUBROUTINES DECOMP AND SOLVE

The subroutines DECOMP(N, IPS, UL) and SOLVE(N, IPS, UL, B, X) solve a system of N linear equations in N unknowns. The input to DECOMP consists of N and the N by N matrix of coefficients on the left-hand side of the matrix equation stored by columns in UL. The output from DECOMP is IPS and UL. This output is fed into solve. The rest of the input to solve consists of N and the column of coefficients on the right-hand side of the matrix equation stored in B. SOLVE puts the solution to the matrix equation in X.

Minimum allocations are given by

COMPLEX UL(N*N)

DIMENSION SCL(N), IPS(N)

in DECOMP and by

COMPLEX UL(N*N), B(N), X(N)

DIMENSION IPS(N)

in SOLVE

More detail concerning DECOMP and SOLVE is on pages 46-49 of [5].

```

1C  LISTING OF THE SUBROUTINE DECOMP
2  SUBROUTINE DECOMP(N,IPS,UL)
3  COMPLEX UL(16),PIVOT,EN
4  DIMENSION SCL(4),IPS(4)
5  DO 5 I=1,N
6  IPS(I)=I
7  RN=0.
8  J1=1
9  DO 2 J=1,N
10  ULH=ABS(REAL(UL(J1)))+ABS(AIMAG(UL(J1)))
11  J1=J1+N
12  IF(RN-ULH) 1,2,2
13  1 RN=ULH
14  2 CONTINUE
15  SCL(1)=1./RN
16  5 CONTINUE
17  NH1=N-1
18  K2=0
19  DO 17 K=1,NH1
20  BIG=0.
21  DO 11 I=K,N
22  IP=IPS(I)
23  IPK=IP+K2
24  SIZE=(ABS(REAL(UL(IPK)))+ABS(AIMAG(UL(IPK))))*SCL(IP)
25  IF(SIZE-BIG) 11,11,10
26  10 BIG=SIZE
27  IPV=I
28  11 CONTINUE
29  IF(IPV-K) 14,15,14
30  14 J=IPS(K)
31  IPS(K)=IPS(IPV)
32  IPS(IPV)=J
33  15 KPP=IPS(K)+K2
34  PIVOT=UL(KPP)
35  KP1=K+1
36  DO 16 I=KP1,N
37  KP=KPP
38  IP=IPS(I)+K2
39  EH=-UL(IP)/PIVOT
40  16 UL(IP)=-EH
41  DO 16 J=KP1,N
42  IP=IP+N
43  KP=KP+N
44  UL(IP)=UL(IP)+EH*UL(KP)
45  16 CONTINUE
46  K2=K2+N
47  17 CONTINUE
48  RETURN
49  END
50C LISTING OF THE SUBROUTINE SOLVE
51 SUBROUTINE SOLVE(N,IPS,UL,B,X)
52 COMPLEX UL(16),B(4),X(4),SUM
53 DIMENSION IPS(4)
54 NP1=N+1
55 IP=IPS(1)
56 X(1)=B(IP)
57 DO 2 I=2,N
58 IP=IPS(I)
59 IPB=IP
60 IM1=I-1
61 SUM=0.
62 DO 1 J=1,IM1
63 SUM=SUM+UL(IP)*X(J)
64 1 IP=IP+N
65 2 X(1)=B(IPB)-SUM
66 K2=N*(N-1)
67 IP=IPS(N)+K2
68 X(N)=X(N)/UL(IP)
69 DO 4 IBACK=2,N
70 I=NP1-IBACK
71 K2=K2-N
72 IP1=IPS(I)+K2
73 IP1=I+1
74 SUM=0.
75 IP=IP1
76 DO 3 J=IP1,N
77 IP=IP+N
78 3 SUM=SUM+UL(IP)*X(J)
79 4 X(1)=(X(1)-SUM)/UL(IP1)
80 RETURN
81 END

```

VIII. THE MAIN PROGRAM

The main program accepts input data from the file MAUTZ3.DAT and writes output data on the file MAUTZ6.DAT. See the open statements on lines 10 and 11 of the listing of the main program at the end of this section. The main program calls the subroutines BES, BESJY, BESJJ, SFEO, DECOMP, and SOLVE. The subroutine SFEO calls the subroutine BESJ. In this section, first the input data are described, then the output data are described, relevant formulas are given, the main program is described verbally, and finally the main program and sample input and output data are listed.

The input data are read early in the main program from the file MAUTZ3.DAT according to

```

                READ(20,25)(Y0(I), I = 1, 36)
25             FORMAT(5E14.7)
                READ(20,28) N1, N2, N3, NA, NR
28             FORMAT(I3, I5, 3I3)
                DO 31 JW = 1, N3
                READ(20,32) NN, IP, IB, X, P, ALP
32             FORMAT(3I3, 3E14.7)
31             CONTINUE

```

The input array Y_0 should not deeply concern the user because he will never have to change it. The values of the elements of Y_0 appear in the sample data listed after the main program. The curious reader will find the values of $Y_0(1)$ to $Y_0(33)$ explained on pages 4 and 5 of [2]. The values of $Y_0(34)$, $Y_0(35)$, and $Y_0(36)$ are $2/\pi$, $\pi/4$, and $3\pi/4$, respectively.

The Bessel functions in the summations in [1, eqs. (41), (42), (47), and (48)] are approximated by Debye's asymptotic expansions whenever $N1 \leq n \leq N2$, and these summations are truncated at $n = N2$. The summations in [1, eqs. (44) and (50)] are truncated at $n = N1-1$. For the z directed electric field $E_z^b(-\underline{M})$ along the straight line that runs from the center of the cylinder to the center of the aperture, the Bessel functions in the first summation in (62) are approximated by Debye's asymptotic expansions whenever $N1 \leq n \leq N2$, and this summation is truncated at $n = N2$.

The aperture field E_z is evaluated at NA equally spaced points in the aperture. Here, $NA \geq 2$. With reference to [1, Fig. 1], the first point is at the beginning of the aperture at $\phi = -\phi_0$, and the NA th point is at the end of the aperture at $\phi = \phi_0$. The interior field $E_z^b(-\underline{M})$ is evaluated at NR equally spaced points along the line that runs from the center of the cylinder to the center of the aperture. Here, $NR \geq 2$. The first point is at the center of the cylinder, and the NR th point is at the center of the aperture.

The NA evaluations of the aperture field and the NR evaluations of the interior field $E_z^b(-\underline{M})$ are done inside DO loop 31, that is, these evaluations are done NN times, once for each value of JW . If $NN = 4$, these fields are obtained by solving [1, eqs. (40) and (46)] in which Y^e and Y^o are, as stated in [1], 4×4 matrices. If $1 \leq NN \leq 3$, the fields are obtained by solving [1, eqs. (40) and (46)] with Y^e replaced by the $NN \times NN$ matrix in its upper left-hand corner, with Y^o replaced by the $NN \times NN$ matrix in its upper left-hand corner, and with \vec{V}^e , \vec{I}^e , and \vec{V}^o , and \vec{I}^o truncated accordingly. We assume that $1 \leq NN \leq 4$.

In DO loop 31, $IP = p$ where p is the non-negative integer upon which the alternative expansion functions [1, eqs. (30) and (34)] depend. The main program was written under the assumption that $IP < N1$. If there is an integer p such that $|J_p(ka)|$ is very small, then the user should take $IP = p$. Here, k is the wave number and a is the radius of the cylinder. However, if there is no value of p such that $|J_p(ka)|$ is very small, a non-negative value of IP must still be chosen, and the alternative expansion functions will be given by [1, eqs. (30) and (34)] with $p = IP$. In this case the fields calculated by the procedure of [1] should not depend on p so that IP can be any non-negative integer less than $N1$. If $IB \neq 0$, then the main program uses the value of $J_{IP}(ka)$ calculated by the subroutine BES. If $IB = 0$, then $J_{IP}(ka)$ is set equal to zero. If the circular cylinder of radius a was resonant such that $J_{IP}(ka) = 0$, then, without IB , it would be virtually impossible to obtain $J_{IP}(ka) = 0$ because the exact resonant value of ka would be difficult to enter, and even if it could be entered, the subroutine BES would probably not give exactly zero for $J_{IP}(ka)$.

In DO loop 31,

$$\left. \begin{array}{l} IP = p \\ X = ka \\ P = \phi_0 \\ ALP = \alpha \end{array} \right\} \quad (16)$$

where p , ka , ϕ_0 , and α appear in [1]. Here, P and ALP are in radians.

The meaning of p was clarified in the previous paragraph, ka is the product of the wave number k and the radius a of the cylinder, ϕ_0 is one half the angular width of the aperture, and α is the value of θ in the direc-

tion from which the incident wave comes. The angles ϕ_0 and α are shown in [1, Fig. 1].

Minimum allocations are given by

```
DIMENSION BJ(MAX(N1*NR, NA)), BY(N1*NR), XR(NR), RP(NR)
```

```
DIMENSION RN(NN*NR), RE(NR), BJJ(NR)
```

where MAX denotes the maximum value.

The main program writes output data on the file MAUTZ6.DAT. The input data of the first two read statements are written out immediately after they are read in.

The following write statements are in DO loop 31:

```

WRITE(21, 27) NN, IP, IB, X, P, ALP
27  FORMAT(' NN=', I3, ', IP=', I3, ', IB = ', I3/
      1' X = ', E14.7, ', P=', E14.7, ', ALP=', E14.7)
WRITE(21, 33) (BJ(NP), NP=JJ, JJN)
33  FORMAT(' BJ'/(1X, 5E14.7))
WRITE(21, 19) (BY(NP), NP = JJ, JJN)
19  FORMAT(' BY'/(1X, 5E14.7))
WRITE(21, 24) (SE(J), J=1, NN)
WRITE(21, 24) (SO(J), J=1, NN)
24  FORMAT(1X, 4E14.7)
WRITE(21, 49) U2, S1
49  FORMAT(' E=', 2E14.7, ', ABS(E) = ', E14.7)
WRITE(21,64) (BJ(L), L = 1, NA)
64  FORMAT(' APERTURE FIELD AMPLITUDE'/(1X, 4E14.7))
WRITE(21, 60)(RE(L), L = 1, NR)
60  FORMAT(' INTERIOR FIELD AMPLITUDE'/(1X, 4E14.7))

```

The above write statements are labeled the first, second, third, ..., eighth write statements. The data of the first write statement are merely input data. The data of the second and third write statements are defined by

$$(BJ(NP), NP = JJ, JJN) = (J_n(ka), n=0,1,\dots, N1-1) \quad (17)$$

$$(BY(NP), NP = JJ, JJN) = (Y_n(ka), n = 0, 1, \dots, N1-1) \quad (18)$$

where $J_n(ka)$ and $Y_n(ka)$ are, respectively, the Bessel functions of the first and second kinds of order n and argument ka . The data of the fourth and fifth write statements are defined by

$$(SE(J), J=1, NN) = (|V_j^e|, j=1,2,\dots, NN) \quad (19)$$

$$(SO(J), J=1, NN) = (|V_j^o|, j=1,2,\dots, NN) \quad (20)$$

where V_j^e appears in [1, eq. (7)] and V_j^o appears in [1, eq. (24)]. If $NN < 4$, then V_j^e and V_j^o are truncated at $j = NN$ because they are given in terms of \hat{V}_j^e and \hat{V}_j^o by [1, eqs. (53) and (54)] and, as indicated earlier, \hat{V}_j^e and \hat{V}_j^o are truncated at $j = NN$.

In the sixth write statement, $U2$ is the complex number whose real and imaginary parts are those of $E_z^b(-\underline{M})$ at the center of the cylinder, and $S1$ is $|E_z^b(-\underline{M})|$ at the center of the cylinder. This $E_z^b(-\underline{M})$ is calculated from [1, eq. (68)]. In the seventh write statement, $BJ(L)$ is the magnitude of the aperture field E_z at $\rho = a$ and $\phi = \phi_L$ where

$$\phi_L = \frac{2(L-1)\phi_o}{NA-1} - \phi_o \quad (21)$$

In the eighth write statement, $RE(L)$ is $|E_z^b(-\underline{M})|$ at $k\rho = k\rho_L$ along the line that runs from the center of the cylinder to the center of the aperture. Here,

$$k\rho_L = \frac{(L-1)ka}{NR-1} \quad (22)$$

This completes our description of the input and output data. The formulas to be programmed are presented next.

Assuming that

$$0 \leq p \leq N1 - 1, \quad (23)$$

we approximate the matrix elements [1, eqs. (41), (42), and (44)] by

$$Y_{il}^e = \frac{F_{ip}^e S_{lp}^e}{H_p^{(2)}(ka)} + J_p(ka) \left[\sum_{\substack{n=0 \\ n \neq p}}^{N1-1} \frac{F_{in}^e S_{ln}^e}{J_n(ka) H_n^{(2)}(ka)} + j \sum_{n=N1}^{N2} \frac{F_{in}^e S_{ln}^e}{J_n(ka) Y_n(ka)} \right], \quad i=1,2,3,4 \quad (24)$$

$$Y_{ij}^e = \sum_{\substack{n=0 \\ n \neq p}}^{N1-1} \frac{F_{in}^e (S_{jn}^e + C_j^e S_{ln}^e)}{J_n(ka) H_n^{(2)}(ka)} + j \sum_{n=N1}^{N2} \frac{F_{in}^e (S_{jn}^e + C_j^e S_{ln}^e)}{J_n(ka) Y_n(ka)}, \quad \begin{cases} i=1,2,3,4 \\ j=2,3,4 \end{cases} \quad (25)$$

$$I_i^e = \sum_{n=0}^{N1-1} \frac{\epsilon_n j^n F_{in}^e \cos(n\alpha)}{H_n^{(2)}(ka)}, \quad i=1,2,3,4 \quad (26)$$

In (25), C_j^e is given by [1, eq. (31)]

$$C_j^e = -\frac{S_{jp}^e}{S_{lp}^e} \quad (27)$$

Expressions (24) and (25) are recast as

$$Y_{il}^e = S_{lp}^e (EF)_{ip} + J_p(ka) \sum_{\substack{n=0 \\ n \neq p}}^{N2} E_{ln}^e (EF)_{in}, \quad i=1,2,3,4 \quad (28)$$

$$Y_{ij}^e = \sum_{\substack{n=0 \\ n \neq p}}^{N2} E_{jn}^e (EF)_{in}, \quad \begin{cases} i=1,2,3,4 \\ j=2,3,4 \end{cases} \quad (29)$$

where

$$(EF)_{in} = \begin{cases} \frac{F_{in}^e}{H_n^{(2)}(ka)}, & n=0,1,\dots,N1-1 \\ j F_{in}^e, & n = N1, N1+1,\dots,N2 \end{cases} \quad (30)$$

$$E_{jn}^e = \begin{cases} \frac{S_{jn}^e + C_j^e S_{1n}^e}{J_n(ka)}, & n=0,1,\dots,p-1,p+1,\dots,N1-1 \\ \frac{S_{jn}^e + C_j^e S_{1n}^e}{J_n(ka) Y_n(ka)}, & n=N1, N1+1,\dots,N2 \end{cases} \quad (31)$$

$$C_j^e = \begin{cases} 0, & j=1 \\ -\frac{S_{jp}^e}{S_{1p}^e}, & j=2,3,4 \end{cases} \quad (32)$$

Assuming that (23) holds, we approximate the matrix elements

[1, eqs. (47), (48), and (50)] by

$$Y_{il}^o = \frac{F_{ip}^o S_{1p}^o}{H_p^{(2)}(ka)} + J_p^o(ka) \left[\sum_{\substack{n=1 \\ n \neq p}}^{N1-1} \frac{F_{in}^o S_{1n}^o}{J_n(ka) H_n^{(2)}(ka)} + j \sum_{n=N1}^{N2} \frac{F_{in}^o S_{1n}^o}{J_n(ka) Y_n(ka)} \right], \quad i=1,2,3,4 \quad (33)$$

$$Y_{ij}^o = \sum_{\substack{n=1 \\ n \neq p}}^{N1-1} \frac{F_{in}^o (S_{jn}^o + C_j^o S_{1n}^o)}{J_n(ka) H_n^{(2)}(ka)} + j \sum_{n=N1}^{N2} \frac{F_{in}^o (S_{jn}^o + C_j^o S_{1n}^o)}{J_n(ka) Y_n(ka)}, \quad \begin{cases} i=1,2,3,4 \\ j=2,3,4 \end{cases} \quad (34)$$

$$I_i^o = 2 \sum_{n=1}^{N1-1} \frac{j^n F_{in}^o \sin(n\alpha)}{H_n^{(2)}(ka)}, \quad i=1,2,3,4 \quad (35)$$

where

$$J_p^o(ka) = \begin{cases} 1, & p = 0 \\ J_p(ka), & p > 0 \end{cases} \quad (36)$$

and [1, eq. (35)]

$$C_j^o = \begin{cases} 0, & p = 0 \\ -\frac{S_{jp}^o}{S_{1p}^o}, & p > 0 \end{cases} \quad (37)$$

Expressions (33) and (34) are recast as

$$Y_{il}^o = S_{lp}^o(OF)_{ip} + J_p^o(ka) \sum_{\substack{n=0 \\ n \neq p}}^{N2} E_{ln}^o(OF)_{in}, \quad i=1,2,3,4 \quad (38)$$

$$Y_{ij}^o = \sum_{\substack{n=0 \\ n \neq p}}^{N2} E_{jn}^o(OF)_{in}, \quad \begin{cases} i=1,2,3,4 \\ j=2,3,4 \end{cases} \quad (39)$$

where

$$(OF)_{in} = \begin{cases} \frac{F_{in}^o}{H_n^{(2)}(ka)}, & n=0,1,\dots,N1-1 \\ j F_{in}^o, & n=N1,N1+1,\dots,N2 \end{cases} \quad (40)$$

$$E_{jn}^o = \begin{cases} \frac{S_{jn}^o + C_j^o S_{1n}^o}{J_n(ka)}, & n=0,1,\dots,p-1,p+1,\dots,N1-1 \\ \frac{S_{jn}^o + C_j^o S_{1n}^o}{J_n(ka) Y_n(ka)}, & n=N1,N1+1,\dots,N2 \end{cases} \quad (41)$$

$$C_j^o = \begin{cases} 0 & , p = 0, j=1,2,3,4 \\ 0 & , p > 0, j=1 \\ \begin{matrix} S_{jp}^o \\ -\frac{j p}{S_{1p}^o} \end{matrix} & , p > 0, j=2,3,4 \end{cases} \quad (42)$$

The terms for which $n=0$ do not contribute to (38) and (39) because $S_{j0}^o = F_{i0}^o = 0$ [1, eqs. (27) and (49)]. The terms for which $n=0$ have been added to make (38) and (39) similar to (28) and (29) and thus easier to program.

For convenience, [1, eqs. (40), (46), and (53)] are repeated here:

$$Y^e \vec{V}^e = \vec{I}^e \quad (43)$$

$$Y^o \vec{V}^o = \vec{I}^o \quad (44)$$

$$\left. \begin{aligned} v_1^e &= J_p(ka) \hat{v}_1^e + \sum_{i=2}^4 C_i^e \hat{v}_i^e \\ v_j^e &= \hat{v}_j^e, \quad j=2,3,4 \end{aligned} \right\} \quad (45)$$

With $J_p^o(ka)$ given by (36) and C_j^o by (42), [1, eqs. (54) and (55)] combine:

$$\left. \begin{aligned} v_1^o &= J_p^o(ka) \hat{v}_1^o + \sum_{i=2}^4 C_i^o \hat{v}_i^o \\ v_j^o &= \hat{v}_j^o, \quad j=2,3,4 \end{aligned} \right\} \quad (46)$$

Expression [1, eq. (68)] for the field $E_z^b(-\underline{M})$ at the center of the cylinder is

$$[E_z^b(-\underline{M})]_{\rho=0} = \begin{cases} S_{10}^e \hat{v}_1^e & , p = 0 \\ \frac{1}{J_o(ka)} \sum_{j=1}^4 S_{jo}^e v_j^e & , p \neq 0 \end{cases} \quad (47)$$

The aperture field E_z is the ϕ component of \underline{M} of [1, eq. (4)]:

$$E_z = M^e + M^o \quad (48)$$

Substituting [1, eqs. (7) and (24)] into (48), using [1, eqs. (8) and (25)], and evaluating E_z at $\phi = \{\phi_L, L = 1, 2, \dots, NA\}$ where ϕ_L is given by (21), we obtain

$$[E_z]_L = \left[\sum_{j=1}^4 \left(\frac{\phi_L}{\phi_o} v_j^o + v_j^e \right) \left(\frac{\phi_L}{\phi_o} \right)^{2j-2} \right] \sqrt{1 - \left(\frac{\phi_L}{\phi_o} \right)^2}, \quad L=1, 2, \dots, NA \quad (49)$$

Along the line from the center of the cylinder to the center of the aperture, $\phi = 0$ so that expression [1, eq. (62)] for the interior field $E_z^b(-\underline{M})$ reduces to

$$E_z^b(-\underline{M}) = \sum_{n=0}^{\infty} \frac{B_n^e J_n(ko)}{J_n(ka)} \quad (50)$$

where B_n^e is given by [1, eqs. (63) or (65)].

$$B_n^e = \begin{cases} \sum_{j=1}^4 v_j^e S_{jn}^e, & n \neq p \\ J_p(ka) \hat{v}_1^e S_{1p}^e, & n=p \end{cases} \quad (51)$$

Truncating the summation in (50) at $n = N2$, substituting (51) into (50), and then letting $k\rho = \{k\rho_L, L=1, 2, \dots, NR\}$ where $k\rho_L$ is given by (22), we have

$$[E_z^b(-\underline{M})]_L = S_{1p}^e J_p(k\rho_L) \hat{v}_1^e + \sum_{j=1}^4 v_j^e \left(\sum_{\substack{n=0 \\ n \neq p}}^{N2} \frac{S_{jn}^e J_n(k\rho_L)}{J_n(ka)} \right), \quad L=1, 2, \dots, NR \quad (52)$$

Expression (52) is recast as

$$[E_z^b(-\underline{M})]_L = (RP)_L \hat{v}_1^e + \sum_{j=1}^4 (RN)_{jL} v_j^e, \quad L = 1, 2, \dots, NR \quad (53)$$

where

$$(RP)_L = S_{1p}^e J_p(k\rho_L) \quad (54)$$

$$(RN)_{jL} = \sum_{\substack{n=0 \\ n \neq p}}^{N1-1} \frac{S_{jn}^e J_n(k\rho_L)}{J_n(ka)} + \sum_{n=N1}^{N2} \frac{S_{jn}^e J_n(k\rho_L)}{J_n(ka)} \quad (55)$$

Expression (55) was obtained by assuming that (23) holds. We plan to use Debye's asymptotic expansions for the Bessel functions in the second summation in (55).

If $L=1$, then $k\rho_L = 0$ and (53) reduces to

$$[E_z^b(-M)]_1 = \begin{cases} S_{10}^e \hat{v}_1^e & , p = 0 \\ \sum_{j=1}^4 \left(\frac{S_{j0}^e}{J_0(ka)} \right) v_j^e & , p \neq 0 \end{cases} \quad (56)$$

Therefore, any difference between the computed values of the field (47) at the center of the cylinder and the field (53) at $L = 1$ is due to roundoff error.

If $L = NR$, then $k\rho_L = ka$ and (52) reduces to

$$[E_z^b(-M)]_{NR} = S_{1p}^e J_p(ka) \hat{v}_1^e + \sum_{j=1}^4 v_j^e \left(\sum_{\substack{n=0 \\ n \neq p}}^{N2} S_{jn}^e \right) \quad (57)$$

Using (45) to express $J_p(ka) \hat{v}_1^e$ in terms of $\{v_j^e, j=1,2,3,4\}$, we obtain

$$J_p(ka) \hat{v}_1^e = v_1^e - \sum_{i=2}^4 C_i^e v_i^e \quad (58)$$

In view of (32), substitution of (58) into (57) gives

$$[E_z^b(-M)]_{NR} = \sum_{j=1}^4 v_j^e \left(\sum_{n=0}^{N2} S_{jn}^e \right) \quad (59)$$

Equating [1, eqs. (8) and (12)] at $\phi = 0$, we obtain

$$\sum_{n=0}^{\infty} S_{jn}^e = \begin{cases} 1 & , j=1 \\ 0 & , j=2,3,4 \end{cases} \quad (60)$$

If

$$\sum_{n=0}^{N/2} S_{jn}^e = \sum_{n=0}^{\infty} S_{jn}^e \quad (61)$$

then (60) would reduce (59) to

$$[E_z^b(-M)]_{NR} = V_1^e \quad (62)$$

If NA is odd so that $\phi_L = 0$ when $L = (NA+1)/2$, then (49) gives

$$[E_z]_L = V_1^e, \quad L = (NA+1)/2 \quad (63)$$

Noting that (62) and (63) have the same right-hand side and recalling that (61) was used to obtain (62), we deduce that any difference between the computed values of the aperture field (49) at the center of the aperture and the interior field (53) at $k\rho_L = ka$ is due to the error in truncating the summation with respect to n in (55), the error in calculating $\{S_{jn}^e\}$, and, of course, roundoff error.

Having presented relevant formulas, we begin to verbally describe the main program. In the equations that were presented in this section, Y^e and Y^o are 4×4 matrices, \vec{V}^e , \vec{I}^e , \vec{V}^o , and \vec{I}^o are 4×1 column vectors, and $\{V_j^e, V_j^o, j=1,2,3,4\}$ are defined by (45) and (46). The equations that were programmed are those that were presented in this section with the order 4 replaced by NN, that is, Y^e and Y^o are replaced by the $NN \times NN$ submatrices in their upper left-hand corners, and \hat{V}_j^e , I_j^e , \hat{V}_j^o , I_j^o , V_j^e , and V_j^o are retained only for $j \leq NN$. We describe the main program by relating variables therein to quantities that appear in the previous text of this section. What follows is clarified in Table 1.

Line 27 and DO loop 61 put

$$J_n(0) = \begin{cases} 1, & n = 0 \\ 0, & n > 0 \end{cases} \quad (64)$$

in BJ(n+1) for $n=0,1,\dots,N1-1$. Equation (64) can be obtained from [3, formula 9.1.10]. In DO loop 18, line 38 puts $J_n(k\rho_L)$ in BJ(n+1+(L-1)*N1) for $n=0,1,\dots,N1-1$ where $k\rho_L$ is given by (22). Line 38 also puts $Y_n(k\rho_L)$ in BY(n+1+(L-1)*N1) for $n=0,1,\dots,N1-1$ although only $\{Y_n(k\rho_{NR}) = Y_n(ka), n=0,1,\dots,N1-1\}$ is needed.

Table 1. Key lines in the main program, the variables read in, defined, or incremented therein, the corresponding quantities in the text, and the numbers of the equations where these quantities appear.

Line Number	Variable(s) in the main program	Quantity in the text	Equation number(s)
22	IP and X	p and ka	16
22	P and ALP	ϕ_o and α in radians	16
27	BJ(1)	$J_o(0)$	55
29	BJ(NP)	$J_{NP-1}(0)$	55
31	XR(1)	$k\rho_1$	22
35	XR(L)	$k\rho_L$	22
38	{BJ(n+JJ), n=0, 1, ..., N1-1}	{ $J_n(k\rho_L)$, n=0, 1, ..., N1-1}	26, 30, 31, 54, 55
38	{BY(n+JJ), n=0, 1, ..., N1-1}	{ $Y_n(k\rho_L)$, n=0, 1, ..., N1-1}	26, 30
61	{SE(J), J=1, 2, 3, 4}	{ S_{Jp}^e , J=1, 2, 3, 4}	32
61	{SO(J), J=1, 2, 3, 4}	{ S_{Jp}^o , J=1, 2, 3, 4}	42
62	BJPE	$J_p(ka)$	28
63	CE(1)	C_1^e	32
66	CE(J)	C_J^e	32

Line Number	Variable(s) in the main program	Quantity in the text	Equation Number(s)
69	BJPO	$J_p^0(ka)$ for $p=0$	36
71	CO(J)	C_J^0 for $p=0$	42
74	BJPO	$J_p^0(ka)$ for $p>0$	36
75	CO(1)	C_1^0 for $p>0$	42
78	CO(J)	C_J^0 for $p>0$	42
84	N	n	26,30,31
85	{SE(J), J=1,2,3,4}	$\{S_{Jn}^e, J=1,2,3,4\}$	31
85	{SO(J), J=1,2,3,4}	$\{S_{Jn}^o, J=1,2,3,4\}$	41
85	{FE(I), I=1,2,3,4}	$\{F_{In}^e, I=1,2,3,4\}$	26,30
85	{FO(I), I=1,2,3,4}	$\{F_{In}^o, I=1,2,3,4\}$	35,40
88	BJN	$J_n(ka)$	26,30
91	U2	$1/H_n^{(2)}(ka)$	26,30
93,94	CSA	$\epsilon_n \cos(n\alpha)$	26
95	SNA	$2 \sin(n\alpha)$	35
97	EF(I)	$F_{In}^e/H_n^{(2)}(ka)$	30
98	OF(I)	$F_{In}^o/H_n^{(2)}(ka)$	40
99	CUE(I)	nth term	26
100	CUO(I)	nth term	35
105	YE(I)	$S_{lp}^e(EF)_{Ip}$	28
106	YO(I)	$S_{lp}^o(OF)_{Ip}$	38
110	RP(L)	$(RP)_L$	54
116	BJJ(L)	$J_n(k_{oL})/J_n(ka)$	55
120	BJN	$J_n(ka) Y_n(ka)$	31,41
122	EF(I)	jF_{In}^e	30
123	OF(I)	jF_{In}^o	40

Line Number	Variable(s) in the main program	Quantity in the Text	Equation number(s)
125	{BJJ(L), L=1,2,...,NR}	$\{J_n(k\rho_L)/J_n(ka)\}$	55
128,131	E	E_J	67
129,132	O	O_J	68
135	YE(IY)	nth term	28 or 29
136	YO(IY)	nth term	38 or 39
143	RN(JR)	nth term	55
148,152	{VE(J), I=1,2,...,NN}	$\{\hat{V}_I^e, I=1,2,...,NN\}$	43
149,154	{VO(I), I=1,2,...,NN}	$\{\hat{V}_I^o, I=1,2,...,NN\}$	44
163	VO(1)	V_1^o	46
164	U3	\hat{V}_1^e	43
165	VE(1)	V_1^e	45
167	SE(J)	$ V_J^e $	45
168	SO(J)	$ V_J^o $	46
173	SE(J)	$\{S_{J0}^e, J=1,2,3,4\}$	47
175	U2	$S_{10}^e \hat{V}_1^e$	47
181	U2	$[E_z^b(-\underline{M})]_{\rho=0}$	47
188	XX	ϕ_L/ϕ_o	49
192	U2	$[E_z]_L$	49
195	BJ(L)	$ [E_z]_L $	49
201	U2	$(RP)_L \hat{V}_1^e$	53
204	U2	$[E_z^b(-\underline{M})]_L$	53
206	RE(L)	$ [E_z^b(-\underline{M})]_L $	53

Line 61 puts S_{Jp}^e of (32) in $SE(J)$ for $J=1,2,3$, and 4. Line 61 also puts S_{Jp}^o of (42) in $SO(J)$ for $J=1,2,3$, and 4. Lines 62 to 67 put $J_p(ka)$ of (28) in $BJPE$ and $\{C_J^e, J=1,2,\dots,NN\}$ of (32) in $\{CE(J), J=1,2,\dots,NN\}$. Lines 68 to 79 put $J_p^o(ka)$ of (33) in $BJPO$ and $\{C_J^o, J=1,2,\dots,NN\}$ of (42) in $\{CO(J), J=1,2,\dots,NN\}$.

Being summations with respect to n , the matrix elements I_I^e of (26), Y_{IJ}^e of (28) and (29), I_I^o of (35), Y_{IJ}^o of (38) and (39), and $(RN)_{JL}$ of (55) are accumulated in $CUE(I)$, $YE(IY)$, $CUO(I)$, $YO(IY)$, and $RN(JR)$, respectively, where

$$\left. \begin{aligned} IY &= I + (J-1)*NN \\ JR &= J + (L-1)*NN \end{aligned} \right\} \quad (65)$$

In DO loop 15,

$$N = NP-1 \quad (66)$$

where NP is the index of DO loop 15. The terms for which $n=N$ are added to $CUE(I)$ and $CUO(I)$ in DO loop 15. If $N \neq p$, then the terms for which $n=N$ are added to $YE(IY)$, $YO(IY)$, and $RN(JR)$ in DO loop 15. If $N=p$, then $S_{1p}^e(EF)_{Ip}$ is added to $YE(I)$, $S_{1p}^o(OF)_{Ip}$ is added to $YO(I)$, and $(RP)_L$ of (54) is put in $RP(L)$ in DO loop 15. More detail on the workings of DO loop 15 is presented in the following four paragraphs.

Line 85 puts S_{Jn}^e of (31) in $SE(J)$, and S_{Jn}^o of (41) in $SO(J)$ for $J=1,2,3$, and 4. Line 85 also puts F_{In}^e of (26) and (30) in $FE(I)$, and F_{In}^o of (35) and (40) in $FO(I)$ for $I=1,2,3$ and 4.

If $N < N1$, then lines 87 to 118 are executed. Line 88 puts $J_n(ka)$ in BJN , line 91 puts $1/H_n^{(2)}(ka)$ in $U2$, lines 93 and 94 put $\epsilon_n \cos(n\alpha)$ in CSA , and line 95 puts $2\sin(n\alpha)$ in SNA . In DO loop 40, $(EF)_{In}$ of (30) is

put in $EF(I)$, $(OF)_{In}$ of (40) is put in $OF(I)$, the n th term of (26) is added to $CUE(I)$, and the n th term of (35) is added to $CUO(I)$. If $N=p$, then DO loops 41 and 53 are executed. In DO loop 41, $S_{1p}^e(EF)_{Ip}$ of (28) is added to $YE(I)$, and $S_{1p}^o(OF)_{Ip}$ of (38) is added to $YO(I)$. In DO loop 53, $(RP)_L$ of (54) is put in $RP(L)$. If $N \neq p$, then DO loop 55 is executed. In DO loop 55, the factor $J_n(k\rho_L)/J_n(ka)$ in the first summation in (55) is put in $BJJ(L)$.

If $N \geq N1$, then lines 120 to 125 are executed. Line 120 puts $J_n(ka) Y_n(ka)$ of (31) and (41) in BJN . DO loop 51 puts jF_{In}^e of (30) in $EF(I)$ and jF_{In}^o of (40) in $OF(I)$. In line 125, the factor $J_n(k\rho_L)/J_n(ka)$ in the second summation in (55) is put in $BJJ(L)$ for $L=1,2,\dots,NR$.

If $N \neq p$, then lines 126 to 145 are executed. Immediately before these lines are executed $(EF)_{In}$ of (30) will reside in $EF(I)$, and $(OF)_{In}$ of (40) will reside in $OF(I)$. Upon entry into DO loop 44, the quantity E_j defined by

$$E_j = \begin{cases} J_p(ka) E_{jn}^e, & j = 1 \\ E_{jn}^e, & j \neq 1 \end{cases} \quad (67)$$

resides in E and the quantity O_j defined by

$$O_j = \begin{cases} J_p^o(ka) E_{jn}^o, & j = 1 \\ E_{jn}^o, & j \neq 1 \end{cases} \quad (68)$$

resides in O . Here, E_{jn}^e is given by (31) and E_{jn}^o by (41). In DO loop 44, the n th term of the summation in (28) or (29) is added to $YE(IY)$, and the n th term of the summation in (38) or (39) is added to $YO(IY)$. In nested DO loops 56 and 57, the n th term of the summation in $(RN)_{JL}$ of (55) is added to $RN(JR)$.

Lines 147 to 154 put the elements of the solution \vec{V}^e of (43) in VE and the elements of the solution \vec{V}^o of (44) in V0. In DO loop 45, V_1^e of (45) is accumulated in U2 and V_1^o of (46) is accumulated in U3. The series in (45) and (46) were, as indicated in the paragraph preceding (64), summed for i up to NN rather than 4. After lines 163-165 have been executed, the elements of \vec{V}^e will reside in VE, the elements of \vec{V}^o will reside in V0, and \hat{V}_1^e will be in U3. In DO loop 47, $|V_J^e|$ is put in SE(J), and $|V_J^o|$ is put in SO(J).

The rest of the main program, lines 173 to 210, serves to calculate the field (47) at the center of the cylinder, the aperture field (49), and the field (53) along the line from the center of the cylinder to the center of the aperture. The series in (47), (49), and (53) are summed with i running from 1 to NN rather than from 1 to 4.

Line 173 puts S_{J0}^e in SE(J) for $J=1,2,3,4$. If $p=0$, then line 175 puts $S_{10}^e \hat{V}_1^e$ of (47) in U2. If $p \neq 0$, then DO loop 48 is executed and line 181 puts $[E_z^b(-M)]_{p=0}$ of (47) in U2.

The index L of DO loop 62 obtains the subscript L in (49). Line 188 puts (ϕ_L/ϕ_0) in XX. DO loop 63 accumulates $[E_z]_L$ of (49) in U2. Line 195 puts $|[E_z]_L|$ of (49) in BJ(L).

The index L of DO loop 58 obtains the subscript L in (53). Line 201 puts $(RP)_L \hat{V}_1^e$ of (53) in U2. DO loop 59 adds to U2 the summation with respect to j in (53). Line 206 puts $|[E_z^b(-M)]_L|$ of (53) in RE(L).

Sample input and output data appear after the listing of the main program. The sample input data are for a perfectly conducting circular cylindrical shell of electrical radius $ka = 2$ with a slot of half angular width $\phi_0 = 1.25^\circ = 0.02181662$ radians centered at $\phi = 0^\circ$ illuminated by a TM plane wave that comes from the direction in which $\phi = 0^\circ$. The last

number in the sixth from the last row of the sample output data is exactly the same as the first number in the last row. This is expected because expression (56) is identical to expression (47) when $p=0$.

We ran the main program with IP of the input data changed from 0 to 1. The first four significant figures of each number in the last six lines of the resulting output data were the same as those that were obtained with $IP=0$. According to (56) and (47), the last number in the sixth from the last line of the output data may, due to roundoff error, be slightly different from the first number in the last line if $IP \neq 0$. These two numbers were identical to each other in the output obtained with $IP=1$.

Note that the third number in the fourth from the last line of the sample output data is slightly different from the last number in the last row. Reasons for this are given in the paragraph that contains (63).


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1 C   LISTING OF THE MAIN PROGRAM
2 C   INPUT DATA ARE READ FROM THE FILE MAUTZ3.DAT ON UNIT 20.
3 C   OUTPUT DATA ARE WRITTEN ON THE FILE MAUTZ6.DAT ON UNIT 21.
4 C   THE SUBROUTINES BES, BESJ, BESJY, BESJJ, SFE0,
5 C   DECOMP, AND SOLVE ARE USED.
6     COMPLEX YE(16),YO(16),CUE(4),CUO(4),U3,U,U2,EF(4),OF(4)
7     COMPLEX VE(4),VO(4)
8     DIMENSION YO(36),BJ(220),BY(220),XR(11),RP(11),RN(44),RE(11)
9     DIMENSION BJJ(11),SE(4),SO(4),FE(4),FO(4),CE(4),CO(4),IPS(4)
10    OPEN(UNIT=20,FILE='MAUTZ3.DAT',STATUS='OLD')
11    OPEN(UNIT=21,FILE='MAUTZ6.DAT',STATUS='OLD')
12    READ(20,25)(YO(I),I=1,36)
13 25  FORMAT(5E14,7)
14    WRITE(21,26)(YO(I),I=1,36)
15 26  FORMAT(' YO'/(1X,5E14,7))
16    READ(20,28) N1,N2,N3,NA,NR
17 28  FORMAT(13,15,313)
18    WRITE(21,29) N1,N2,N3,NA,NR
19 29  FORMAT(' N1=',13,', N2=',15,', N3=',13,', NA=',13,', NR=',13)
20    N1N=N1-1
21    DO 31 JV=1,N3
22    READ(20,32) NN,IP,IB,X,P,ALP
23 32  FORMAT(313,3E14,7)
24    WRITE(21,27) NN,IP,IB,X,P,ALP
25 27  FORMAT(' NN=',13,', IP=',13,', IB=',13/
26    ' X=',E14,7,', P=',E14,7,', ALP=',E14,7)
27    BJ(1)=1.
28    DO 61 NP=2,N1
29    BJ(NP)=0.
30 61  CONTINUE
31    XR(1)=0.
32    JJ=1
33    FNR=NR-1
34    DO 18 L=2,NR
35    XR(L)=(L-1)/FNR*X
36    IF(L.EQ.NR) XR(L)=X
37    JJ=JJ+N1
38    CALL BES(YO,N1N,XR(L),BJ(JJ),BY(JJ))
39 18  CONTINUE
40    JJN=JJ+N1-1
41    WRITE(21,33)(BJ(NP),NP=JJ,JJN)
42 33  FORMAT(' BJ'/(1X,5E14,7))
43    WRITE(21,19)(BY(NP),NP=JJ,JJN)
44 19  FORMAT(' BY'/(1X,5E14,7))
45    NN2=NN*NN
46    DO 35 I=1,NN2
47    YE(I)=0.
48    YO(I)=0.
49 35  CONTINUE
50    DO 36 I=1,NN
51    CUE(I)=0.
52    CUO(I)=0.
53 36  CONTINUE

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```

54     NRN=NR*NN
55     DO 52 J=1,NRN
56     RN(J)=0.
57 52 CONTINUE
58     N1R=N1*(NR-1)
59     IPP=IP+1+N1R
60     IF(1B.EQ.0) BJ(IPP)=0.
61     CALL SFEO(IP,P,SE,SO,FE,FO)
62     BJPE=BJ(IPP)
63     CE(1)=0.
64     IF(NN.EQ.1) GO TO 34
65     DO 37 J=2,NN
66     CE(J)=-SE(J)/SE(1)
67 37 CONTINUE
68 34 IF(IP.NE.0) GO TO 21
69     BJPO=1.
70     DO 38 J=1,NN
71     CO(J)=0.
72 38 CONTINUE
73     GO TO 23
74 21 BJPO=BJPE
75     CO(1)=0.
76     IF(NN.EQ.1) GO TO 23
77     DO 22 J=2,NN
78     CO(J)=-SO(J)/SO(1)
79 22 CONTINUE
80 23 U3=(1.,0.)
81     U=(0.,1.)
82     N2P=N2+1
83     DO 15 NP=1,N2P
84     N=NP-1
85     CALL SFEO(N,P,SE,SO,FE,FO)
86     IF(N.GE.N1) GO TO 50
87     NPN=NP+N1R
88     BJN=BJ(NPN)
89     S1=BJN
90     IF(ABS(S1).LE.1.E-10) S1=0.
91     U2=1./CMPLX(S1,-BY(NPN))
92     ALN=ALP*N
93     CSA=2.*COS(ALN)
94     IF(N.EQ.0) CSA=1.
95     SNA=2.*SIN(ALN)
96     DO 40 I=1,NN
97     EF(I)=FE(I)*U2
98     OF(I)=FO(I)*U2
99     CUE(I)=CSA*EF(I)*U3+CUE(I)
100    CUO(I)=SNA*OF(I)*U3+CUO(I)
101 40 CONTINUE
102    U3=U3*U
103    IF(N.NE.IP) GO TO 20
104    DO 41 I=1,NN
105    YE(I)=SE(I)*EF(I)+YE(I)
106    YO(I)=SO(I)*OF(I)+YO(I)

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107 41 CONTINUE
108    IJ=NP
109    DO 53 L=1,NR
110      RP(L)=SE(1)*BJ(IJ)
111      IJ=IJ+N1
112 53 CONTINUE
113    GO TO 15
114 20 JJ=NP
115    DO 55 L=1,NR
116      BJJ(L)=BJ(JJ)/BJN
117      JJ=JJ+N1
118 55 CONTINUE
119    GO TO 54
120 50 CALL BESJY(N,X,BJN)
121    DO 51 I=1,NN
122      EF(I)=FE(I)*U
123      OF(I)=FO(I)*U
124 51 CONTINUE
125    CALL BESJJ(N,NR,XR,BJJ)
126 54 IY=0
127    DO 42 J=1,NN
128      E=(SE(J)+CE(J)*SE(1))/BJN
129      O=(SO(J)+CO(J)*SO(1))/BJN
130      IF(J.NE.1) GO TO 43
131      E=BJPE+E
132      O=BJPO+O
133 43 DO 44 I=1,NN
134      IY=IY+1
135      YE(IY)=E*EF(I)+YE(IY)
136      YO(IY)=O*OF(I)+YO(IY)
137 44 CONTINUE
138 42 CONTINUE
139    JR=0
140    DO 56 L=1,NR
141      DO 57 J=1,NN
142        JR=JR+1
143        RN(JR)=BJJ(L)*SE(J)+RN(JR)
144 57 CONTINUE
145 56 CONTINUE
146 15 CONTINUE
147    IF(NN.NE.1) GO TO 17
148    VE(1)=CUE(1)/YE(1)
149    VO(1)=CUO(1)/YO(1)
150    GO TO 16
151 17 CALL DECOMP(NN,IPS,YE)
152    CALL SOLVE(NN,IPS,YE,CUE,VE)
153    CALL DECOMP(NN,IPS,YO)
154    CALL SOLVE(NN,IPS,YO,CUO,VO)
155 16 CE(1)=BJPE
156    CO(1)=BJPO
157    U2=0.
158    U3=0.
159    DO 45 I=1,NN

```

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160      U2=CE(1)*VE(1)+U2
161      U3=CO(1)*VO(1)+U3
162  45 CONTINUE
163      VO(1)=U3
164      U3=VE(1)
165      VE(1)=U2
166      DO 47 J=1,NN
167      SE(J)=CABS(VE(J))
168      SO(J)=CABS(VO(J))
169  47 CONTINUE
170      WRITE(21,24)(SE(J),J=1,NN)
171      WRITE(21,24)(SO(J),J=1,NN)
172  24 FORMAT(1X,4E14.7)
173      CALL SFEO(0,P,SE,SO,FE,FO)
174      IF(IP.NE.0) GO TO 46
175      U2=SE(1)*U3
176      GO TO 39
177  46 U2=0.
178      DO 48 J=1,NN
179      U2=SE(J)*VE(J)+U2
180  48 CONTINUE
181      U2=U2/BJ(N1R+1)
182  39 S1=CABS(U2)
183      WRITE(21,49) U2,S1
184  49 FORMAT(' E=',2E14.7,'. ABS(E)=' ,E14.7)
185      FNA=2./(NA-1)
186      DO 62 L=1,NA
187      U2=0.
188      XX=-1.+(L-1)*FNA
189      X2=XX*XX
190      S1=SQRT(1.-X2)
191      DO 63 J=1,NN
192      U2=S1*(XX*VO(J)+VE(J))+U2
193      S1=S1*X2
194  63 CONTINUE
195      BJ(L)=CABS(U2)
196  62 CONTINUE
197      WRITE(21,64)(BJ(L),L=1,NA)
198  64 FORMAT(' APERTURE FIELD AMPLITUDE'/(1X,4E14.7))
199      JR=0
200      DO 58 L=1,NR
201      U2=RP(L)*U3
202      DO 59 J=1,NN
203      JR=JR+1
204      U2=RM(JR)*VE(J)+U2
205  59 CONTINUE
206      RE(L)=CABS(U2)
207  58 CONTINUE
208      WRITE(21,60)(RE(L),L=1,NR)
209  60 FORMAT(' INTERIOR FIELD AMPLITUDE'/(1X,4E14.7))
210  31 CONTINUE
211      STOP
212      END

```

C

C LISTING OF THE INPUT DATA FILE MAUTZ3.DAT

-0.3072582E+04 0.7368758E+04-0.6085100E+03 0.1710234E+02-0.2271001E+00
 0.1600171E-02-0.5961089E-05 0.9545773E-08 0.4163150E+05 0.3420211E+03
 0.1000000E+01-0.6024727E+04 0.1613512E+04-0.7532210E+02 0.1402590E+01
 -0.1275602E-01 0.5832787E-04-0.1107698E-06 0.3072946E+05 0.2886431E+03
 0.1000000E+01 0.9999999E+00-0.1097659E-02 0.2461455E-04 0.1000000E+01
 0.1829893E-02-0.3191328E-04-0.1562498E-01 0.1427079E-03-0.5937434E-05
 0.4687498E-01-0.1998720E-03 0.7317495E-05 0.6366198E+00 0.7853982E+00
 0.2356194E+01

2010000 1 5 3

4 0 1 0.2000000E+01 0.2181662E-01 0.0000000E+00

C

C LISTING OF THE OUTPUT DATA FILE MAUTZ6.DAT

Y0

-0.3072582E+04 0.7368758E+04-0.6085100E+03 0.1710234E+02-0.2271001E+00
 0.1600171E-02-0.5961089E-05 0.9545773E-08 0.4163150E+05 0.3420211E+03
 0.1000000E+01-0.6024727E+04 0.1613512E+04-0.7532210E+02 0.1402590E+01
 -0.1275602E-01 0.5832787E-04-0.1107698E-06 0.3072946E+05 0.2886431E+03
 0.1000000E+01 0.9999999E+00-0.1097659E-02 0.2461455E-04 0.1000000E+01
 0.1829893E-02-0.3191328E-04-0.1562498E-01 0.1427079E-03-0.5937434E-05
 0.4687498E-01-0.1998720E-03 0.7317495E-05 0.6366198E+00 0.7853982E+00
 0.2356194E+01

N1= 20, N2=10000, N3= 1, NA= 5, NR= 3

NN= 4, IP= 0, IB= 1

X= 0.2000000E+01, P= 0.2181662E-01, ALP= 0.0000000E+00

BJ

0.2238908E+00 0.5767248E+00 0.3528340E+00 0.1289432E+00 0.3399571E-01
 0.7039629E-02 0.1202429E-02 0.1749441E-03 0.2217955E-04 0.2492343E-05
 0.2515386E-06 0.2304285E-07 0.1932695E-08 0.1494942E-09 0.1072946E-10
 0.7183016E-12 0.4506005E-13 0.2659308E-14 0.1481737E-15 0.7819242E-17

BY

0.5103757E+00-0.1070324E+00-0.6174081E+00-0.1127784E+01-0.2765943E+01
 -0.9935989E+01-0.4691401E+02-0.2715481E+03-0.1853922E+04-0.1455983E+05
 -0.1291846E+06-0.1277286E+07-0.1392096E+08-0.1657742E+09-0.2141144E+10
 -0.2981024E+11-0.4450125E+12-0.7090389E+13-0.1200916E+15-0.2154558E+16
 0.4655501E-01 0.1714323E-01 0.6358480E-01 0.5726649E-01
 0.0000000E+00 0.0000000E+00 0.0000000E+00 0.0000000E+00

E=-0.1121177E-02-0.2728021E-03, ABS(E)= 0.1153889E-02

APERTURE FIELD AMPLITUDE

0.0000000E+00 0.4136272E-01 0.4655501E-01 0.4136272E-01
 0.0000000E+00

INTERIOR FIELD AMPLITUDE

0.1153889E-02 0.1597396E-02 0.4656652E-01

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- [2] J. R. Mautz and R. F. Harrington, "Computer Programs for Electromagnetic Scattering from a Slotted TM Cylindrical Conductor by the Pseudo-Image Method," Technical Report SYRU/DECE/TR-85/5, Department of Electrical and Computer Engineering, Syracuse University, Syracuse, NY 13244-1240, Nov. 1985.
- [3] M. Abramowitz and I. A. Stegun, Handbook of Mathematical Functions, U. S. Government Printing Office, Washington, D.C. (Natl. Bur. Std. U.S. Applied Math. Ser. 55), 1964.
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- [5] J. R. Mautz and R. F. Harrington, "Transmission from a Rectangular Waveguide into Half Space through a Rectangular Aperture," Technical Report TR-76-5, Department of Electrical and Computer Engineering, Syracuse University, Syracuse, NY 13244-1240, May 1976.

END

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